

Chapter Outline: Phase Diagrams

Microstructure and Phase Transformations in Multicomponent Systems

- Definitions and basic concepts
- Phases and microstructure
- Binary isomorphous systems (complete solid solubility)
- Binary eutectic systems (limited solid solubility)
- Binary systems with intermediate phases/compounds
- The iron-carbon system (steel and cast iron)

Definitions: Components and Phases

Component - chemically recognizable species (Fe and C in carbon steel, H₂O and Sucrose in sugar solution in water). A **binary** alloy contains two components, a **ternary** alloy – three, etc.

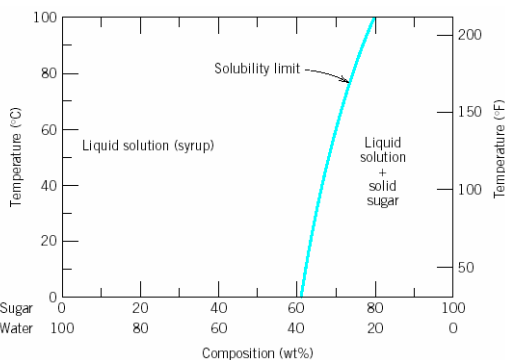
Phase – a portion of a system that has uniform physical **and** chemical characteristics. Two distinct phases in a system have distinct physical and/or chemical characteristics (e.g. water and ice, water and oil) and are separated from each other by definite **phase boundaries**. A phase may contain one or more components.

A single-phase system is called **homogeneous**, systems with two or more phases are **mixtures** or **heterogeneous** systems.

Definitions: Solubility Limit

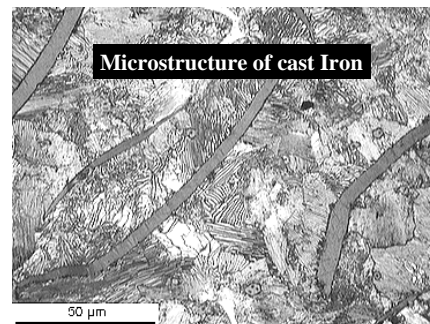
Solvent - host or major component in solution, **solute** - minor component.

Solubility Limit of a component in a phase is the maximum amount of the component that can be dissolved in it (e.g. alcohol has unlimited solubility in water, sugar has a limited solubility, oil is insoluble). The same concepts apply to solid phases: Cu and Ni are mutually soluble in any amount (unlimited solid solubility), while C has a limited solubility in Fe.



Microstructure

The properties of an alloy depend not only on proportions of the phases but also on how they are arranged structurally at the microscopic level. Thus, the microstructure is specified by the number of phases, their proportions, and their arrangement in space.

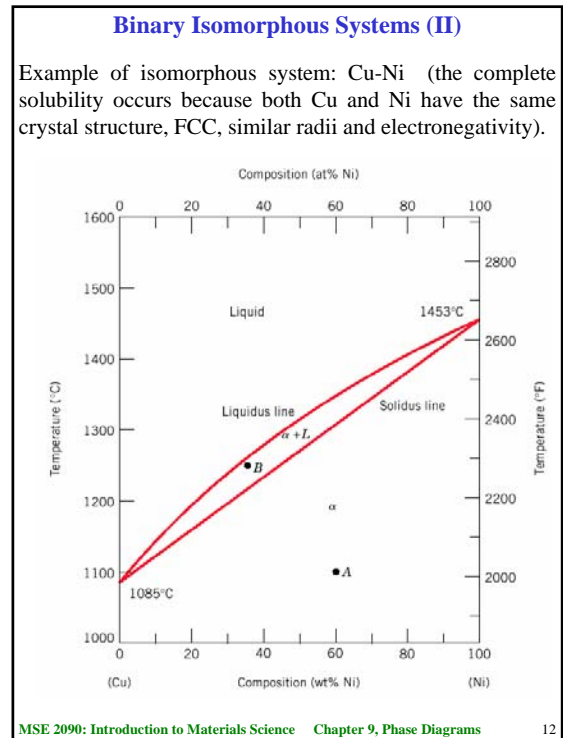
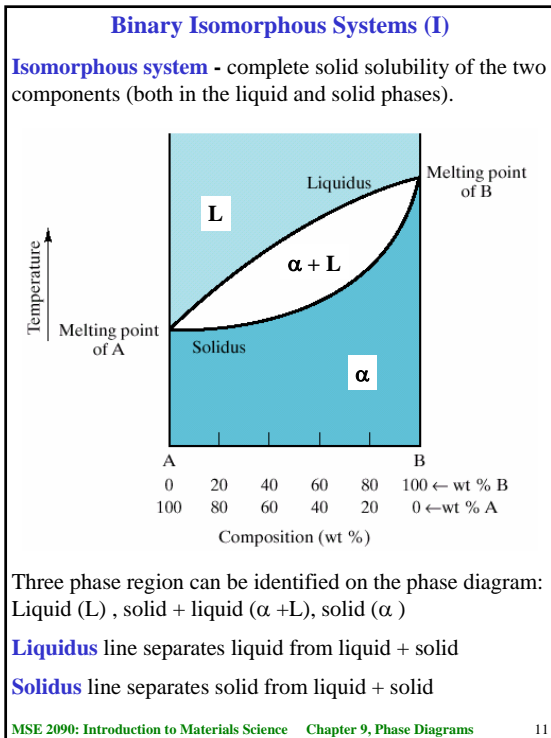
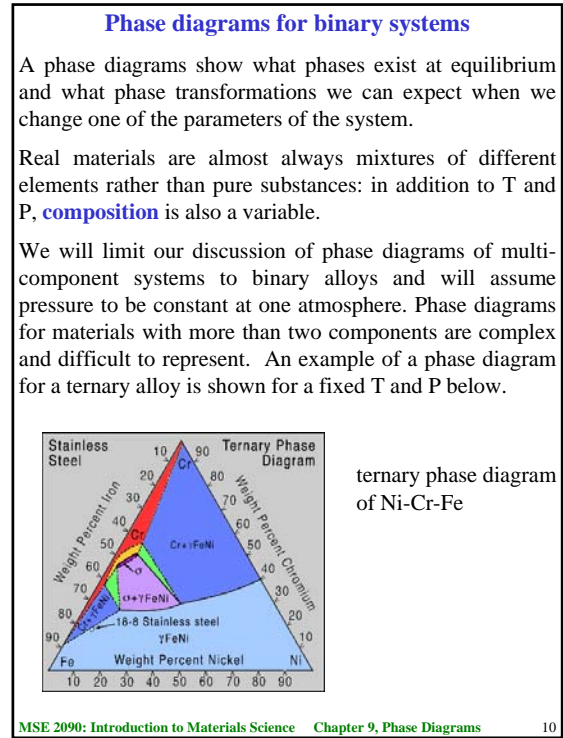
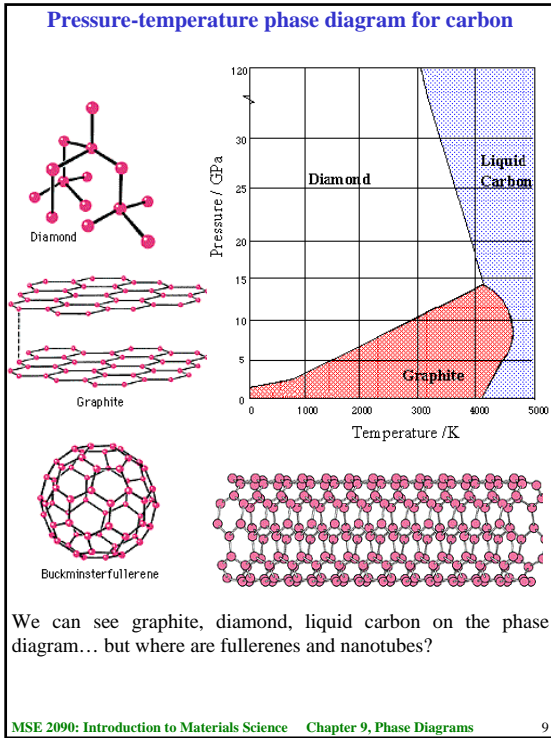


<http://www2.umist.ac.uk/material/research/intmic/> (link is dead)

The long gray regions are flakes of graphite.

The matrix is a fine mixture of BCC Fe and Fe₃C compound.

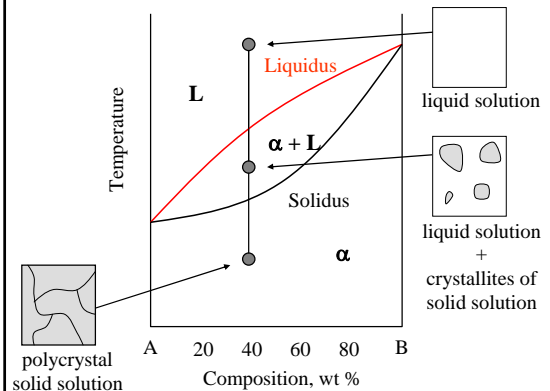
Phase diagrams will help us to understand and predict microstructures like the one shown in this page



Binary Isomorphous Systems (III)

In one-component system melting occurs at a well-defined melting temperature.

In multi-component systems **melting occurs over the range of temperatures**, between the solidus and liquidus lines. Solid and liquid phases are at equilibrium with each other in this temperature range.



Interpretation of a binary phase diagrams

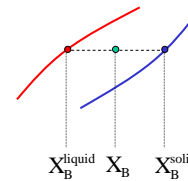
For a given temperature and composition we can use phase diagram to determine:

- 1) The phases that are present
- 2) Compositions of the phases
- 3) The relative fractions of the phases

Finding the composition in a two phase region:

1. Locate composition and temperature in diagram
2. In two phase region draw the **tie line** or isotherm
3. Note intersection with phase boundaries. Read compositions at the intersections.

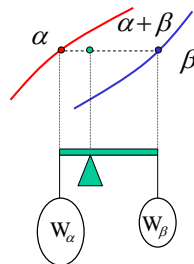
The liquid and solid phases have these compositions.



The lever rule

Finding the amounts of phases in a two phase region:

1. Locate composition and temperature in diagram
2. In two phase region draw the tie line or isotherm
3. Fraction of a phase is determined by taking the length of the tie line to the phase boundary for the **other phase**, and dividing by the total length of tie line



The lever rule is a mechanical analogy to the mass balance calculation. The tie line in the two-phase region is analogous to a lever balanced on a fulcrum.

Derivation of the lever rule

- 1) All material must be in one phase or the other:

$$W_{\alpha} + W_L = 1$$

- 2) Mass of a component that is present in both phases equal to the mass of the component in one phase + mass of the component in the second phase:

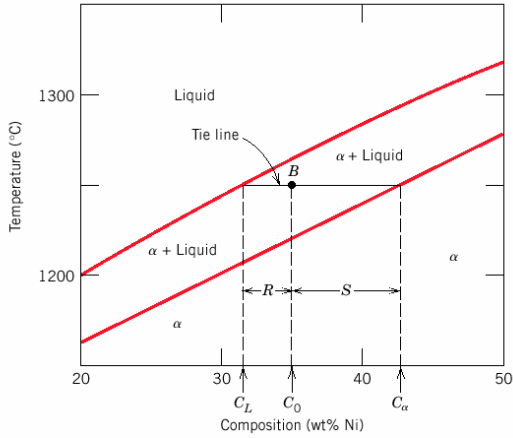
$$W_{\alpha}C_{\alpha} + W_L C_L = C_o$$

- 3) Solution of these equations gives us the lever rule.

$$W_L = (C_{\alpha} - C_o) / (C_{\alpha} - C_L)$$

$$W_{\alpha} = (C_o - C_L) / (C_{\alpha} - C_L)$$

Phase compositions and amounts. An example.



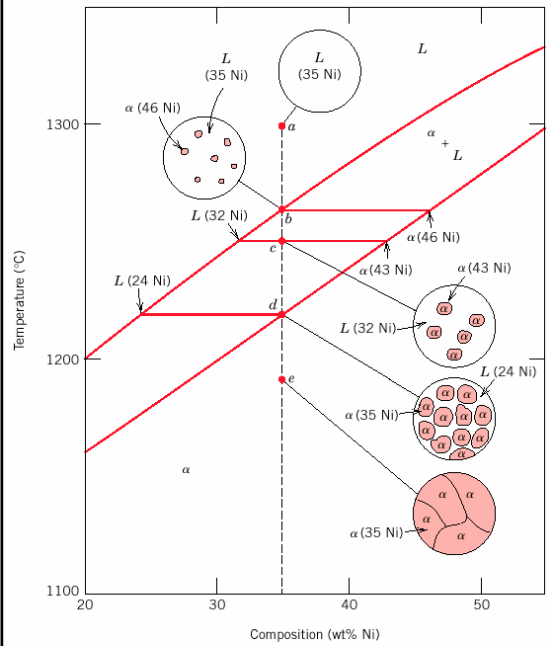
$C_0 = 35 \text{ wt. } \%, C_L = 31.5 \text{ wt. } \%, C_\alpha = 42.5 \text{ wt. } \%$

Mass fractions:

$$W_L = S / (R+S) = (C_\alpha - C_0) / (C_\alpha - C_L) = 0.68$$

$$W_\alpha = R / (R+S) = (C_0 - C_L) / (C_\alpha - C_L) = 0.32$$

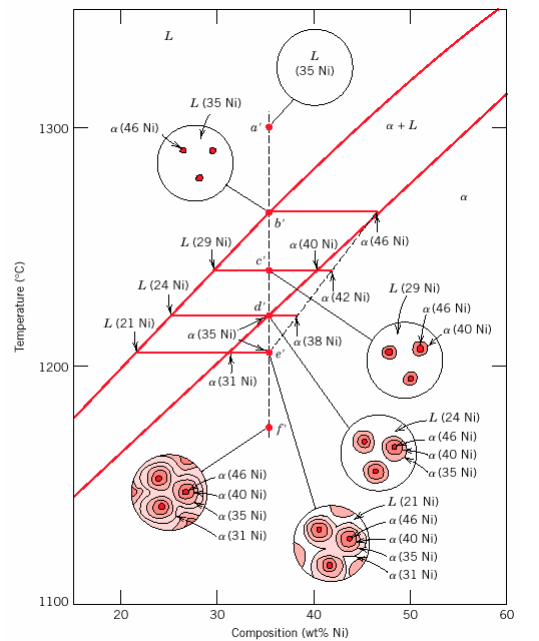
Development of microstructure in isomorphous alloys
Equilibrium (very slow) cooling



Development of microstructure in isomorphous alloys
Equilibrium (very slow) cooling

- Solidification in the solid + liquid phase occurs gradually upon cooling from the liquidus line.
- The composition of the solid and the liquid change gradually during cooling (as can be determined by the tie-line method.)
- Nuclei of the solid phase form and they grow to consume all the liquid at the solidus line.

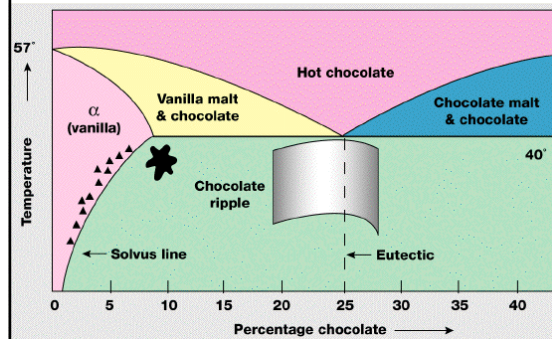
Development of microstructure in isomorphous alloys
Fast (non-equilibrium) cooling



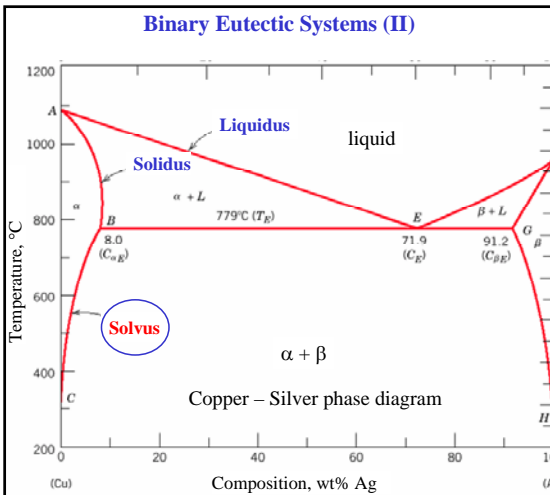
Development of microstructure in isomorphous alloys
Fast (non-equilibrium) cooling

- Compositional changes require diffusion in solid and liquid phases
- Diffusion in the solid state is very slow. \Rightarrow The new layers that solidify on top of the existing grains have the equilibrium composition at that temperature but once they are solid their composition does not change. \Rightarrow Formation of layered (cored) grains and the invalidity of the tie-line method to determine the composition of the solid phase.
- The tie-line method still works for the liquid phase, where diffusion is fast. Average Ni content of solid grains is higher. \Rightarrow Application of the lever rule gives us a greater proportion of liquid phase as compared to the one for equilibrium cooling at the same T. \Rightarrow Solidus line is shifted to the right (higher Ni contents), solidification is complete at lower T, the outer part of the grains are richer in the low-melting component (Cu).
- Upon heating grain boundaries will melt first. This can lead to premature mechanical failure.

Binary Eutectic Systems (I)
systems (alloys) with limited solubility



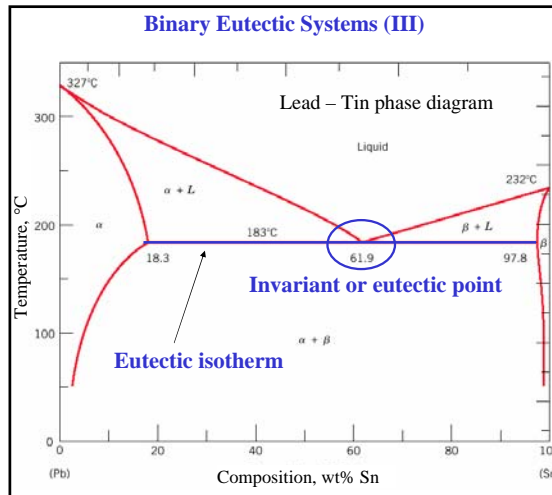
Credit: Kenneth A. Jackson, University of Arizona.



Three single phase regions (α - solid solution of Ag in Cu matrix, β = solid solution of Cu in Ag matrix, L - liquid)

Three two-phase regions ($\alpha + L$, $\beta + L$, $\alpha + \beta$)

Solvus line separates one solid solution from a mixture of solid solutions. **Solvus line shows limit of solubility**



Eutectic or invariant point - Liquid and two solid phases co-exist in equilibrium at the eutectic composition C_E and the eutectic temperature T_E .

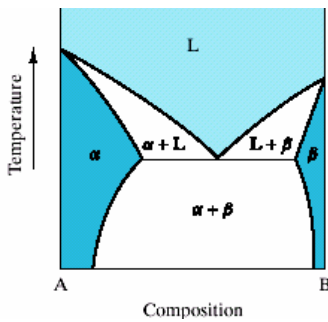
Eutectic isotherm - the horizontal solidus line at T_E .

Binary Eutectic Systems (IV)

Eutectic reaction – transition between liquid and mixture of two solid phases, $\alpha + \beta$ at eutectic concentration C_E .

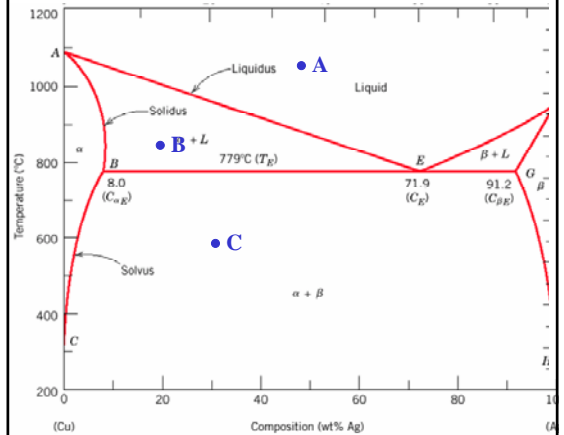
The melting point of the eutectic alloy is lower than that of the components (*eutectic = easy to melt in Greek*).

At most two phases can be in equilibrium within a phase field. Three phases (L, α , β) may be in equilibrium only at a few points along the eutectic isotherm. Single-phase regions are separated by 2-phase regions.



Binary Eutectic Systems (V)

Compositions and relative amounts of phases are determined from the same tie lines and lever rule, as for isomorphous alloys

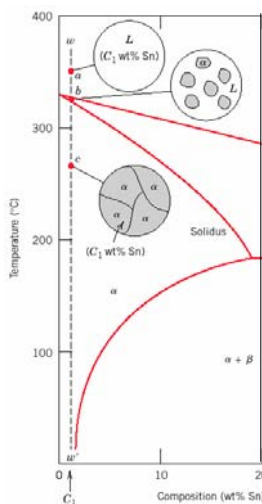


For points A, B, and C calculate the compositions (wt. %) and relative amounts (mass fractions) of phases present.

Development of microstructure in eutectic alloys (I)

Several different types of microstructure can be formed in slow cooling an different compositions.

Let's consider cooling of liquid lead – tin system at different compositions.

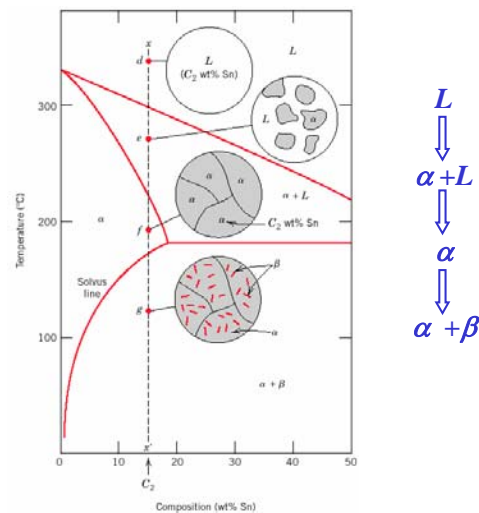


In this case of lead-rich alloy (0-2 wt. % of tin) solidification proceeds in the same manner as for isomorphous alloys (e.g. Cu-Ni) that we discussed earlier.

$$L \rightarrow \alpha + L \rightarrow \alpha$$

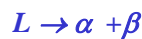
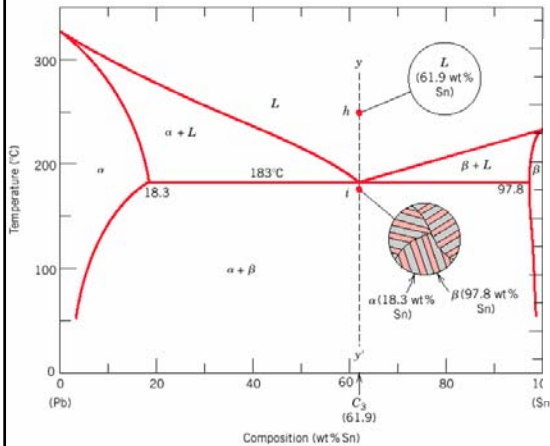
Development of microstructure in eutectic alloys (II)

At compositions between the room temperature solubility limit and the maximum solid solubility at the eutectic temperature, β phase nucleates as the α solid solubility is exceeded upon crossing the solvus line.



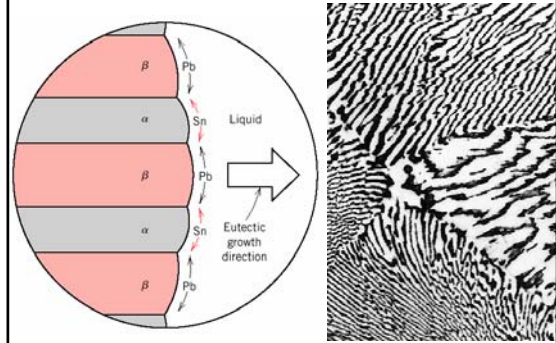
Development of microstructure in eutectic alloys (III)
Solidification at the eutectic composition

No changes above the eutectic temperature T_E . At T_E the liquid transforms to α and β phases (eutectic reaction).



Development of microstructure in eutectic alloys (IV)
Solidification at the eutectic composition

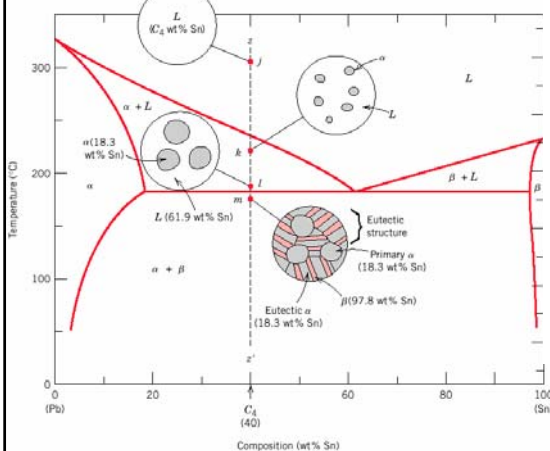
Compositions of α and β phases are very different \rightarrow eutectic reaction involves redistribution of Pb and Sn atoms by atomic diffusion. This simultaneous formation of α and β phases result in a layered (lamellar) microstructure that is called **eutectic structure**.



Formation of the eutectic structure in the lead-tin system. In the micrograph, the dark layers are lead-rich α phase, the light layers are the tin-rich β phase.

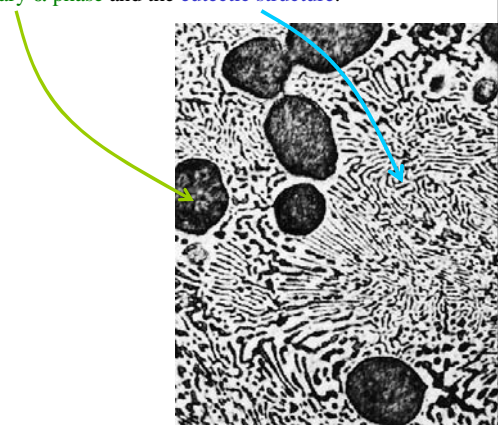
Development of microstructure in eutectic alloys (V)
Compositions other than eutectic but within the range of the eutectic isotherm

Primary α phase is formed in the $\alpha + L$ region, and the eutectic structure that includes layers of α and β phases (called **eutectic α** and **eutectic β** phases) is formed upon crossing the eutectic isotherm.



Development of microstructure in eutectic alloys (VI)

Microconstituent – element of the microstructure having a distinctive structure. In the case described in the previous page, microstructure consists of two microconstituents, **primary α** phase and the **eutectic structure**.



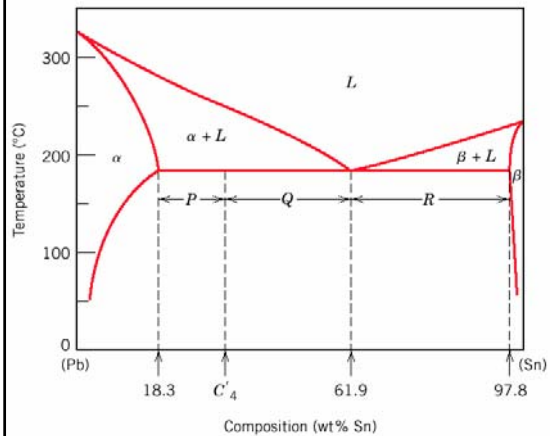
Although the eutectic structure consists of two phases, it is a microconstituent with distinct lamellar structure and fixed ratio of the two phases.

How to calculate relative amounts of microconstituents?

Eutectic microconstituent forms from liquid having eutectic composition (61.9 wt% Sn)

We can treat the eutectic as a separate phase and apply the lever rule to find the relative fractions of primary α phase (18.3 wt% Sn) and the eutectic structure (61.9 wt% Sn):

$$W_e = P / (P+Q) \quad (\text{eutectic}) \quad W_{\alpha'} = Q / (P+Q) \quad (\text{primary})$$



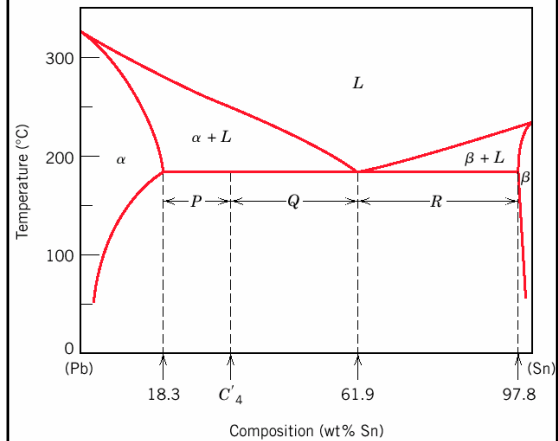
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How to calculate the total amounts of phases?

Fraction of α phase determined by application of the lever rule across the entire $\alpha + \beta$ phase field:

$$W_{\alpha} = (Q+R) / (P+Q+R) \quad (\alpha \text{ phase})$$

$$W_{\beta} = P / (P+Q+R) \quad (\beta \text{ phase})$$



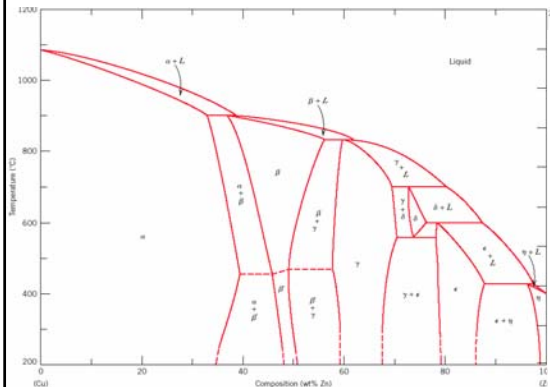
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Phase diagrams with intermediate phases

Eutectic systems that we have studied so far have only two solid phases (α and β) that exist near the ends of phase diagrams. These phases are called **terminal solid solutions**.

Some binary alloy systems have **intermediate solid solution phases**. In phase diagrams, these phases are separated from the composition extremes (0% and 100%).

Example: in Cu-Zn, α and η are terminal solid solutions, $\beta, \beta', \gamma, \delta, \epsilon$ are intermediate solid solutions.

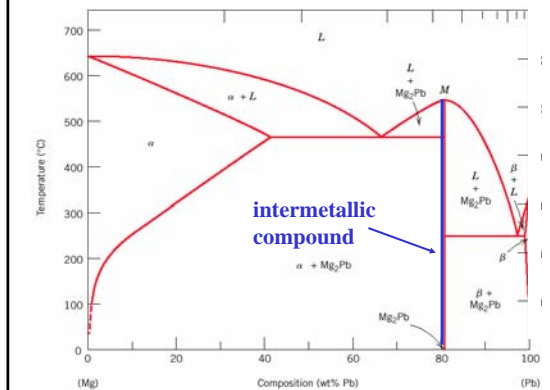


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Phase diagrams with intermetallic compounds

Besides solid solutions, **intermetallic compounds**, that have precise chemical compositions can exist in some systems.

When using the lever rules, intermetallic compounds are treated like any other phase, except they appear not as a wide region but as a vertical line.



This diagram can be thought of as two joined eutectic diagrams, for Mg-Mg₂Pb and Mg₂Pb-Pb. In this case compound Mg₂Pb can be considered as a component.

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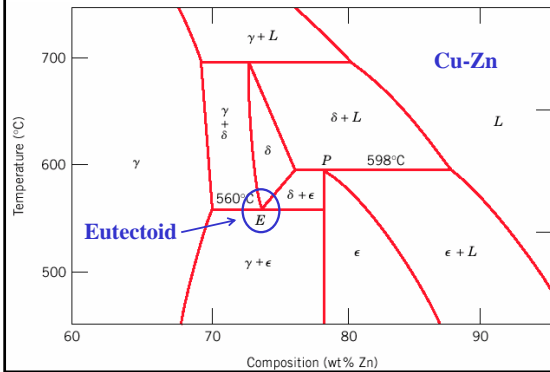
Eutectoid Reactions (I)

The **eutectoid** (*eutectic-like* in Greek) reaction is similar to the eutectic reaction but occurs from one solid phase to two new solid phases.

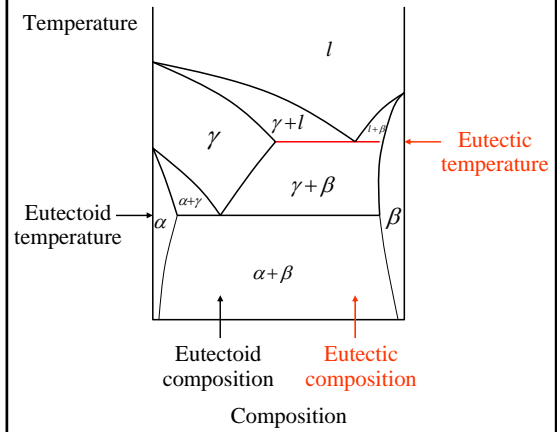
Invariant point (the eutectoid) – three **solid** phases are in equilibrium.

Upon cooling, a solid phase transforms into two other solid phases ($\delta \leftrightarrow \gamma + \epsilon$ in the example below)

Looks as V on top of a horizontal tie line (eutectoid isotherm) in the phase diagram.



Eutectic and Eutectoid Reactions

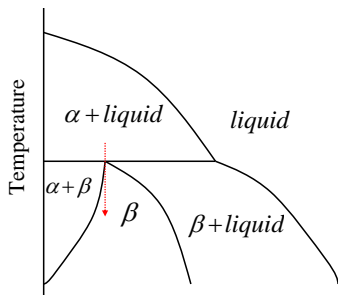


The above phase diagram contains both an eutectic reaction and its solid-state analog, an eutectoid reaction

Peritectic Reactions

A **peritectic** reaction - solid phase and liquid phase will together form a second solid phase at a particular temperature and composition upon cooling, e.g. $L + \alpha \leftrightarrow \beta$

These reactions are rather slow as the product phase will form at the boundary between the two reacting phases thus separating them, and slowing down any further reaction.

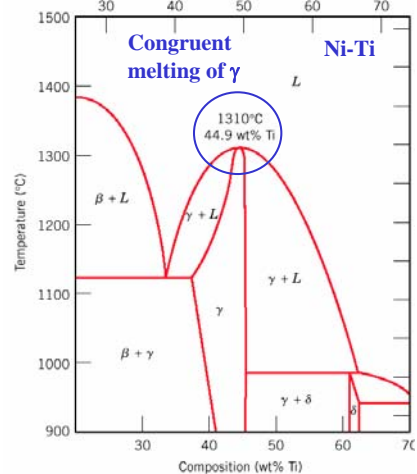


Peritectics are not as common as eutectics and eutectoids, but do occur in some alloy systems. There is one in the Fe-C system that we will consider later.

Congruent phase transformations

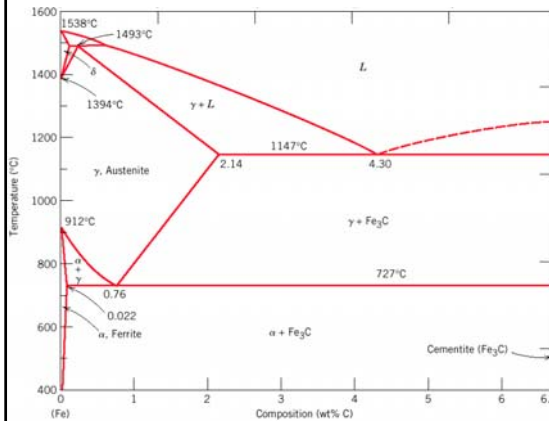
A **congruent transformation** involves no change in composition (e.g., allotropic transformation such as α -Fe to γ -Fe or melting transitions in pure solids).

For an incongruent transformation, at least one phase changes composition (e.g. eutectic, eutectoid, peritectic reactions).



The Iron-Iron Carbide (Fe-Fe₃C) Phase Diagram

In their simplest form, steels are alloys of Iron (Fe) and Carbon (C). The Fe-C phase diagram is a fairly complex one, but we will only consider the steel part of the diagram, up to around 7% Carbon.



Phases in Fe-Fe₃C Phase Diagram

- **α-ferrite - solid solution of C in BCC Fe**
 - Stable form of iron at room temperature.
 - The maximum solubility of C is 0.022 wt%
 - Transforms to FCC γ-austenite at 912 °C
- **γ-austenite - solid solution of C in FCC Fe**
 - The maximum solubility of C is 2.14 wt %.
 - Transforms to BCC δ-ferrite at 1395 °C
 - Is not stable below the eutectoid temperature (727 °C) unless cooled rapidly (Chapter 10)
- **δ-ferrite solid solution of C in BCC Fe**
 - The same structure as α-ferrite
 - Stable only at high T, above 1394 °C
 - Melts at 1538 °C
- **Fe₃C (iron carbide or cementite)**
 - This intermetallic compound is metastable, it remains as a compound indefinitely at room T, but decomposes (very slowly, within several years) into α-Fe and C (graphite) at 650 - 700 °C
- **Fe-C liquid solution**

A few comments on Fe-Fe₃C system

C is an interstitial impurity in Fe. It forms a solid solution with α, γ, δ phases of iron

Maximum solubility in BCC α-ferrite is limited (max. 0.022 wt% at 727 °C) - BCC has relatively small interstitial positions

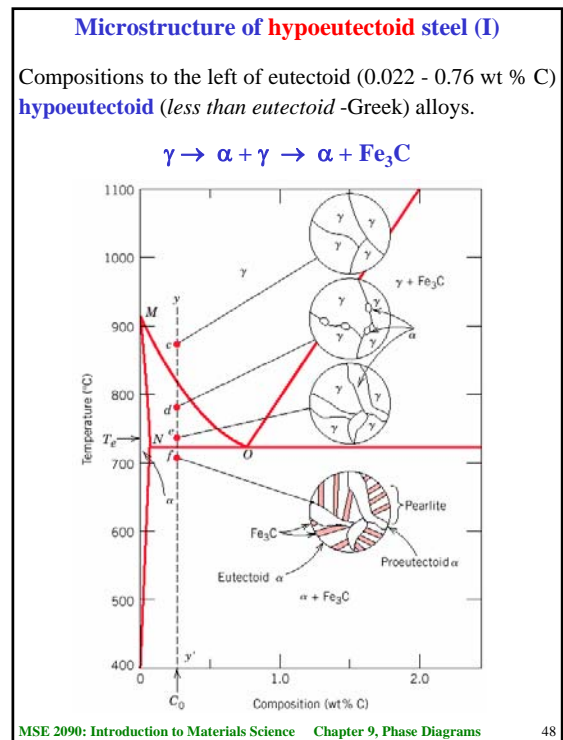
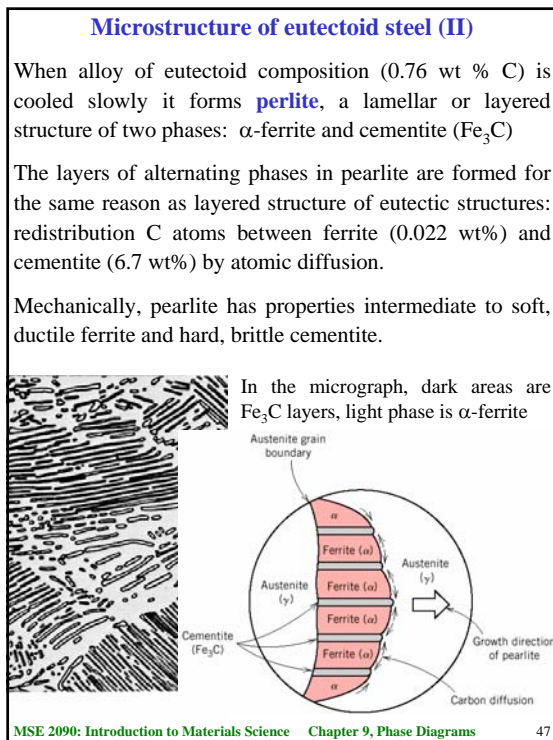
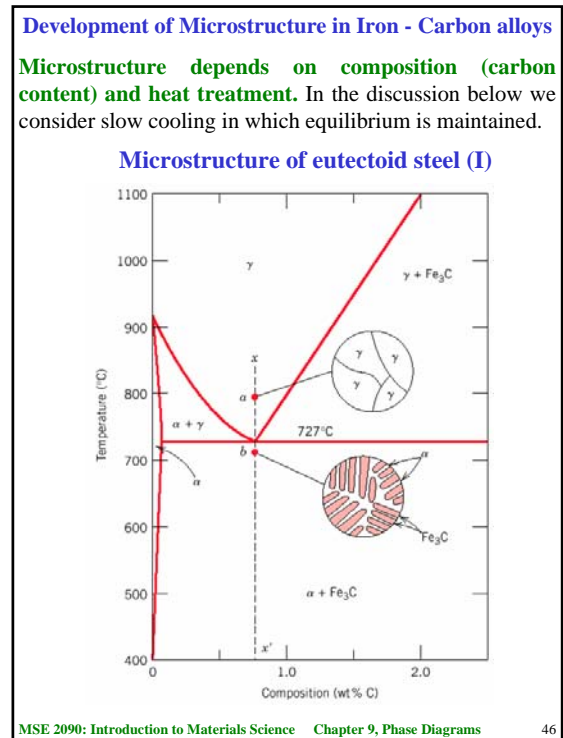
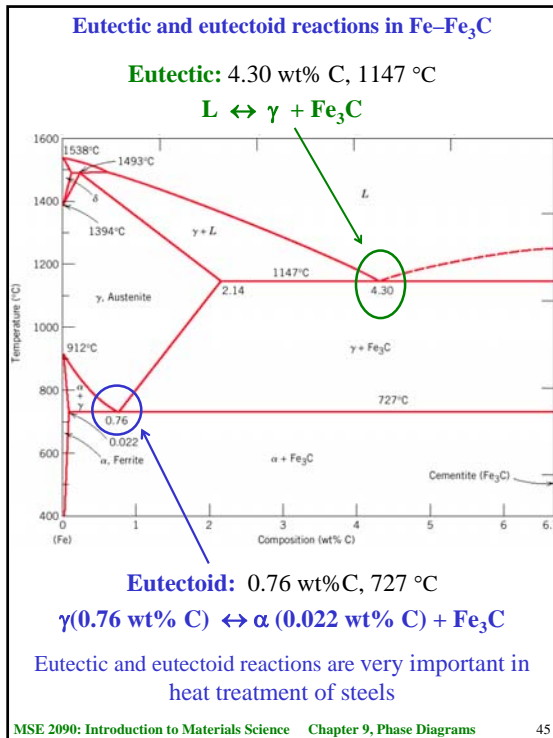
Maximum solubility in FCC austenite is 2.14 wt% at 1147 °C - FCC has larger interstitial positions

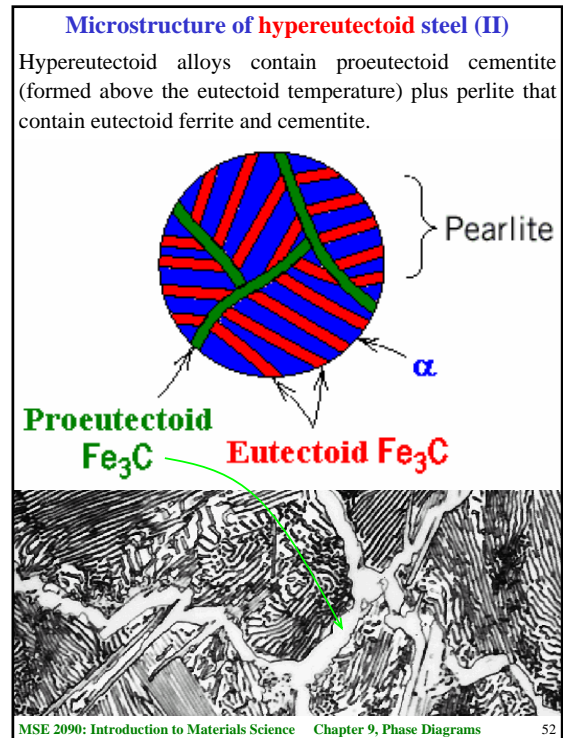
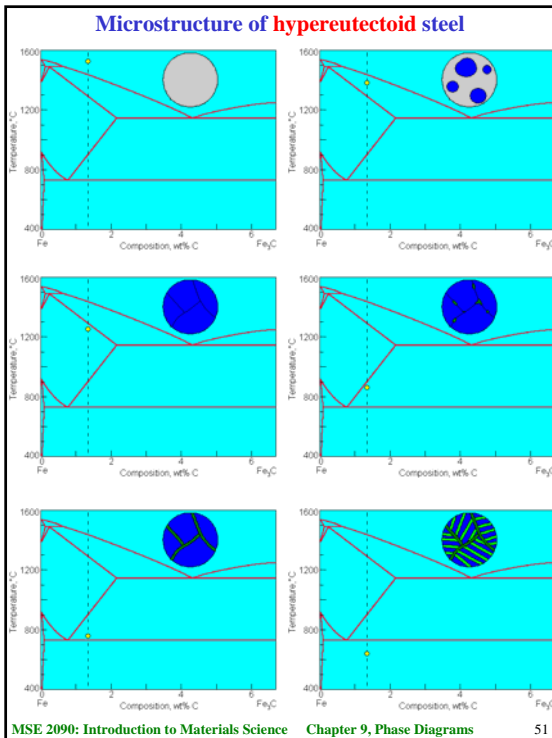
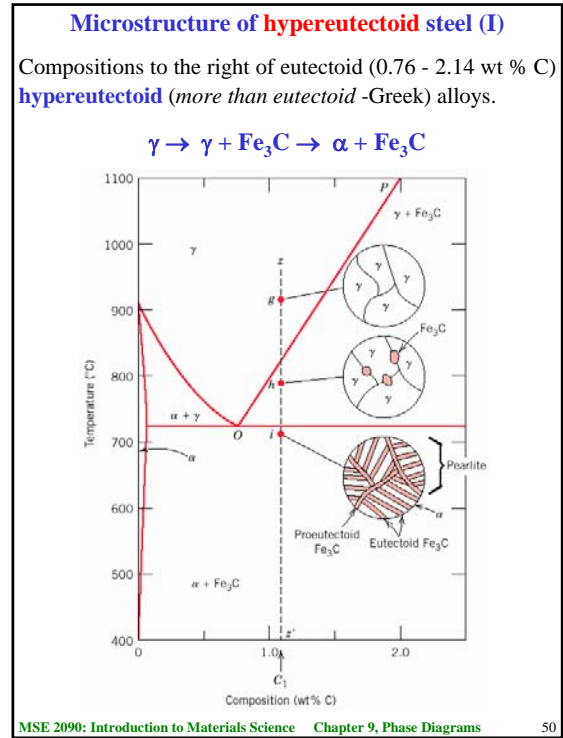
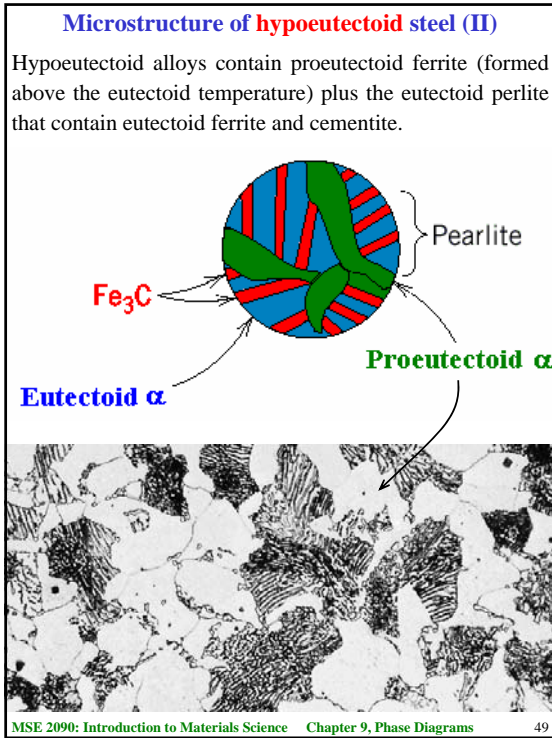
Mechanical properties: Cementite is very hard and brittle - can strengthen steels. Mechanical properties also depend on the microstructure, that is, how ferrite and cementite are mixed.

Magnetic properties: α -ferrite is magnetic below 768 °C, austenite is non-magnetic

Classification. Three types of ferrous alloys

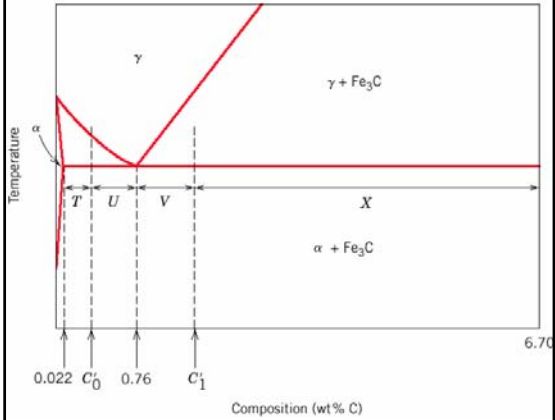
- **Iron:** less than 0.008 wt % C in α-ferrite at room T
- **Steels:** 0.008 - 2.14 wt % C (usually < 1 wt %)
α-ferrite + Fe₃C at room T
Examples of tool steel (tools for cutting other metals):
Fe + 1wt % C + 2 wt % Cr
Fe + 1 wt% C + 5 wt% W + 6 wt % Mo
Stainless steel (food processing equipment, knives, petrochemical equipment, etc.): 12-20 wt% Cr, ~\$1500/ton
- **Cast iron:** 2.14 - 6.7 wt % (usually < 4.5 wt %)
heavy equipment casing





How to calculate the relative amounts of proeutectoid phase (α or Fe_3C) and pearlite?

Application of the lever rule with tie line that extends from the eutectoid composition (0.75 wt% C) to $\alpha - (\alpha + \text{Fe}_3\text{C})$ boundary (0.022 wt% C) for hypoeutectoid alloys and to ($\alpha + \text{Fe}_3\text{C}$) - Fe_3C boundary (6.7 wt% C) for hypereutectoid alloys.



Fraction of α phase is determined by application of the lever rule across the entire ($\alpha + \text{Fe}_3\text{C}$) phase field.

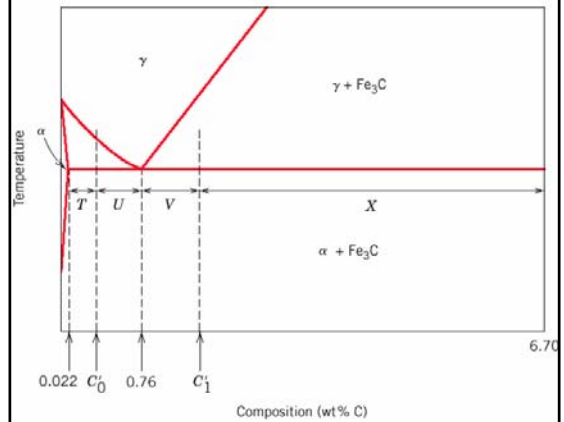
Example for hypereutectoid alloy with composition C_1

Fraction of pearlite:

$$W_P = X / (V+X) = (6.7 - C_1) / (6.7 - 0.76)$$

Fraction of proeutectoid cementite:

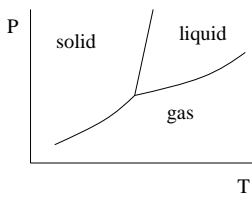
$$W_{\text{Fe}_3\text{C}} = V / (V+X) = (C_1 - 0.76) / (6.7 - 0.76)$$



The Gibbs phase rule

Let's consider a simple one-component system.

In the areas where only one phase is stable both pressure and temperature can be *independently* varied without upsetting the phase equilibrium \rightarrow there are 2 **degrees of freedom**.



Along the lines where two phases coexist in equilibrium, only one variable can be *independently* varied without upsetting the two-phase equilibrium (P and T are related by the Clapeyron equation) \rightarrow there is only one degree of freedom.

At the triple point, where solid liquid and vapor coexist any change in P or T would upset the three-phase equilibrium \rightarrow there are no degrees of freedom.

In general, the number of degrees of freedom, F, in a system that contains C components and can have Ph phases is given by the **Gibbs phase rule**:

$$F = C - Ph + 2$$

The Gibbs phase rule – example of a binary system

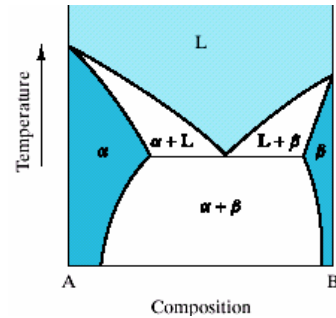
$$F = C - Ph + 2$$

$$P = \text{const}$$

$$F = C - Ph + 1$$

$$C = 2$$

$$F = 3 - Ph$$



\triangleright In one-phase regions of the phase diagram T and X_B can be changed independently.

\triangleright In two-phase regions, $F = 1$. If the temperature is chosen independently, the compositions of both phases are fixed.

\triangleright Three phases (L, α , β) are in equilibrium only at the eutectic point in this two component system ($F = 0$).

Summary

Make sure you understand language and concepts:

- Austenite
- Cementite
- Component
- Congruent transformation
- Equilibrium
- Eutectic phase
- Eutectic reaction
- Eutectic structure
- Eutectoid reaction
- Ferrite
- Gibbs phase rule
- Hypereutectoid alloy
- Hypoeutectoid alloy
- Intermediate solid solution
- Intermetallic compound
- Invariant point
- Isomorphous
- Lever rule
- Liquidus line
- Metastable
- Microconstituent
- Pearlite
- Peritectic reaction
- Phase
- Phase diagram
- Phase equilibrium
- Primary phase
- Proeutectoid cementite
- Proeutectoid ferrite
- Solidus line
- Solubility limit
- Solvus line
- System
- Terminal solid solution
- Tie line