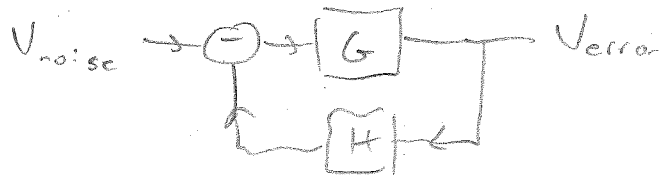


Lecture 14 - Improving Control

More on servos:



Get $V_{err} = \frac{G_0 V_{in}}{1 + G_0 H}$

Want $|1 + G_0 H| \gg 1$ to make V_{err} small

$\Rightarrow |G_0 H| \gg 1$

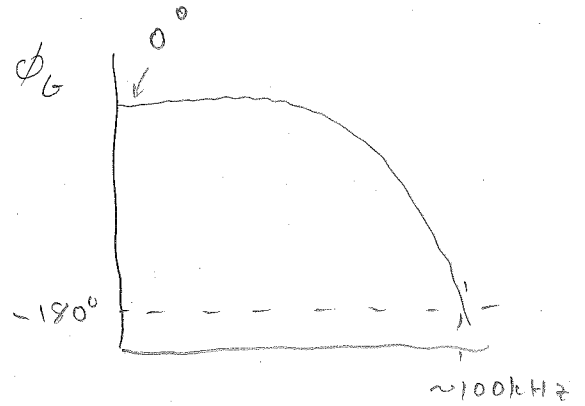
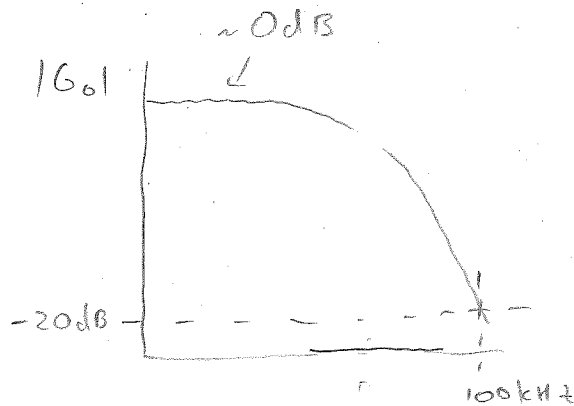
But as $\omega \rightarrow \infty$, $|G_0 H| \rightarrow 0$

and $\phi_{GH} \rightarrow -\infty$

System is stable only if $|G_0 H| < 1$ when $\phi < -180^\circ$

Limits how large H can be

From lab:



Ideally, $H \sim \text{constant}$ and $\phi_H \sim 0^\circ$

So $\phi_{GH} = \phi_G$

Define $f_{180} = \text{freq where } \phi_{GH} \rightarrow -180^\circ$ $f_{180} \approx 100 \text{ kHz}$

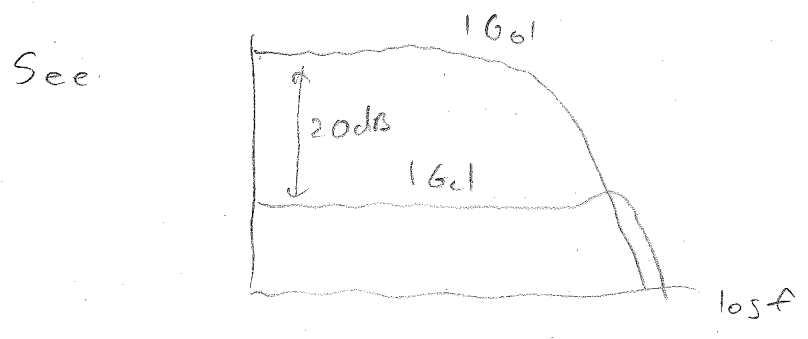
At 100 kHz, $|G_0| = -20 \text{ dB}$

Need $|G_0 H| < 0 \text{ dB} \Rightarrow |H| < 20 \text{ dB}$

Larger H & system starts to oscillate

Then at low frequencies, where $G_0 \approx 1$,

noise reduction is $\frac{1}{1+G_0H} \approx \frac{1}{1+(1)-(10)} = \frac{1}{11} \approx -20\text{dB}$



~ 90% noise reduction, not bad

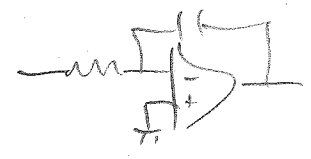
But what if we want to do better?

Key idea; make H frequency dependent

Ideally, H large at low f, drops to 20 dB at f_{180} (since we need $H(f_{180}) < 20\text{dB}$)

For instance, say $H \propto \frac{1}{f}$

Get from integrator



But integrator comes with -90° phase:

$H = \frac{1}{i\omega\tau}$ $\tau = RC$
 $\frac{1}{i} = e^{-i\pi/2}$

We need $|G_0H| < 1$ before $\phi_{GH} = -180^\circ$

$\phi_{GH} = \phi_G + \phi_H$ here = $\phi_G - 90^\circ$

So we need to look at freq where $\phi_G = -90^\circ$, $\equiv f_{90}$

Our circuit has $f_{90} \approx 20\text{kHz}$

$|G(f_{90})| \approx -10\text{dB}$

Still need $|G(f_{90}) H(f_{90})| < 1$

$$-10 \text{ dB} + (H)_{\text{dB}} < 0 \text{ dB}$$

$$\Rightarrow |H(f_{90})| < 10 \text{ dB} = 3 \times$$

$$\text{Have } |H| = \frac{1}{2\pi f \tau}, \text{ so } H(f_{90}) = \frac{1}{2\pi f_{90} \tau} < 3$$

$$\text{So } RC = \tau > \frac{1}{6\pi f_{90}} = 2.6 \mu\text{s}$$

As long as we obey this, system should be stable

But then noise reduction at low f is great!

$$\text{At } f = 60 \text{ Hz}, \quad |H| = \frac{1}{2\pi \cdot 60 \text{ Hz} \cdot 2.6 \mu\text{s}} = 1000 = 60 \text{ dB}$$

$$\text{So noise reduction is } \frac{1}{|2 + G_0 H|} = \frac{1}{|2 + 1 \cdot (1000)|} \approx \frac{1}{1000}$$

Factor of 1000 better than before

Call this "integral control" ("I")

Version with $|H| = \text{const}$ called proportional control ("P")

Integral control pretty much just better

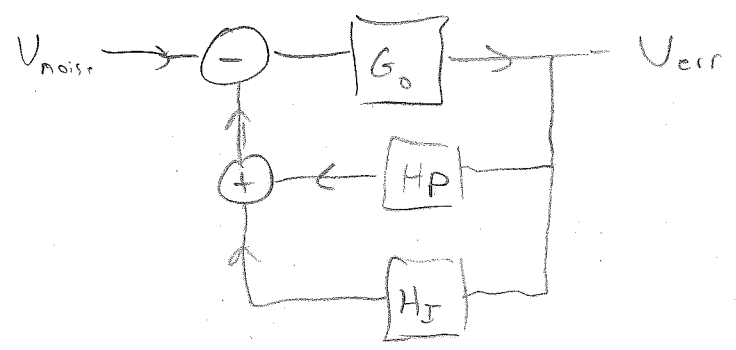
But! sacrifice some noise reduction at high frequencies

at f_{90} , I control has $|G_0 H| < 1$

P control has $|G_0 H| \gg 1$

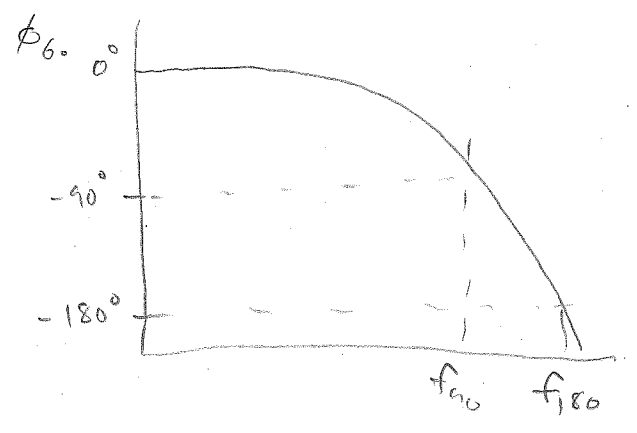
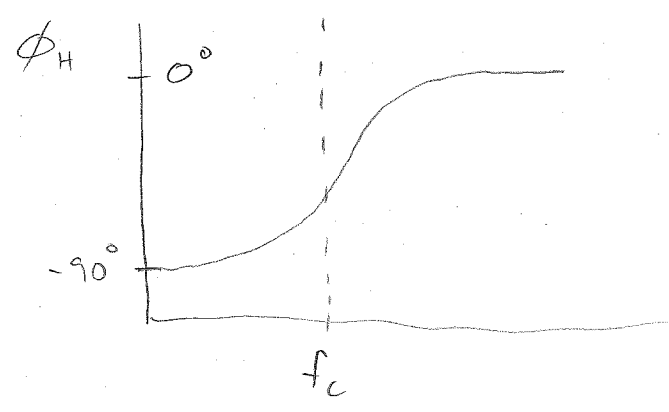
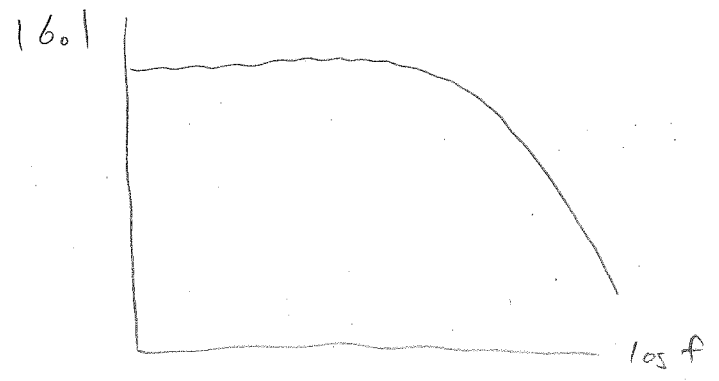
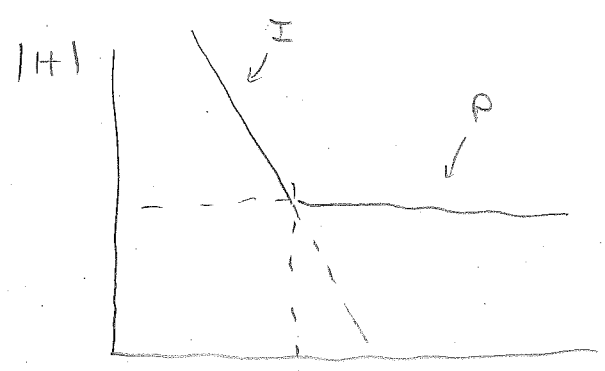
Usually, low frequencies more important

When high freqs do matter, get best of both:
use P + I together!



Called PI control

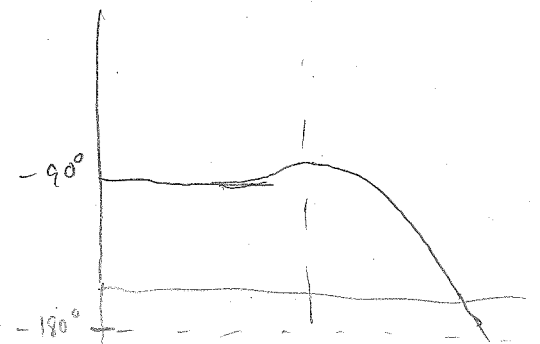
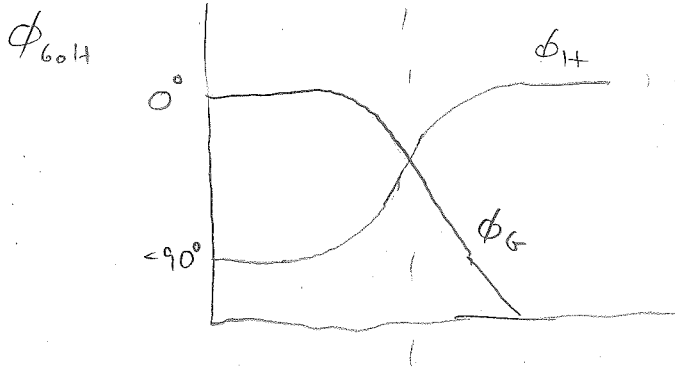
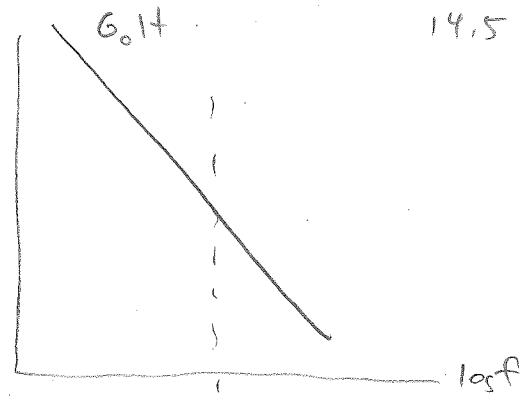
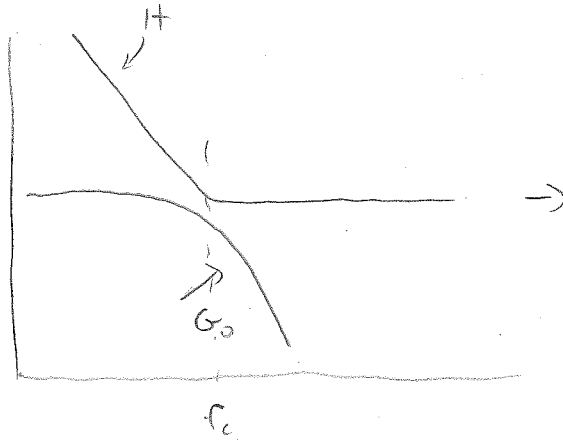
Hard to analyze algebraically, but graphs are useful



- $f_c =$ freq where P + I parts are equal magnitude
- $f_{90} =$ " where $\phi_G = -90^\circ$
- $f_{180} =$ " where $\phi_G = -180^\circ$

Say we make $f_c = f_{90}$

Then $|G_o H|$



As ϕ_G decreases, ϕ_H increases to compensate

Total phase is -180° at f_{180} , same as in P system

So at low freqs, get benefits of I
at high freqs, get benefits of P

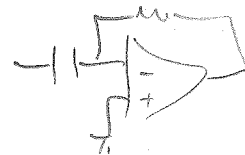
Can extend idea further:

When ϕ_G hits -180° , increase ϕ_H again

Achieve with differentiator

$$H_D = i\omega RC$$

$$\phi = +90^\circ$$



Add this to P+I, get PID controller

Works well if ϕ_G isn't changing too fast near -180°

But often ϕ_G drops fast: f_{270} close to f_{180}

Then derivative control doesn't help much